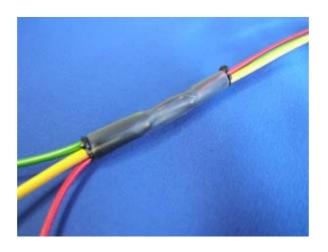


No: PIP-101 Revision:	2	Dated:	January 2012	
-----------------------	---	--------	--------------	--

# Title:- Size Selection & Installation of QSZH-125



Prepared By: Name: Clive Benning Date: January 2012
Reviewed & Approved By: Name: Kurt Joachim Date: January 2012

Note: This document is electronically reviewed and approved - therefore no signature will appear

No: PIP-101 Revision: 2 Dated: January 2012

# **Contents**

		<u>Page</u>
1	Scope	3
2	Revision History/ Reason for Change/ Related Documents	3
3	Introduction	3
4	Splice Design & Preparation Guidelines	4-8
5	Tube Size Selection & Installation Guidelines	9-12
6	Sealing Verification/ Visual Standards	13-16
Appendix 1	General Wire Chart	17-18
Appendix 2	UHI-250A Thermal Probe	19
Appendix 3	Test Methods	20
Appendix 4	Trouble Shooting	21

No:	PIP-101	Revision:	2	Dated:	January 2012
-----	---------	-----------	---	--------	--------------

#### 1 Scope

This document details the important aspects of splice design together with selection and installation criteria when using TE Connectivity QSZH-125 splice sealing products.

#### 2 Revision History / Reason for Change / Related Documents

Rev	Date	Prepared By	Doc Approved By	CR No.
New Product. Initial document.				
1	February 2008	Barry Jenkins	Joao Rocha	New document
2	January 2012	Clive Benning	Kurt Joachim	CR12-DP-041

**Reason for** Review content and update product references.

Revision:

**Related** TE Connectivity Flier - RBK-ILS-MK2 No. TFAE0043

**Documents:** Processor

Maintenance & Repair Manual THFIT/MR/020

TE Connectivity Flier - Seal Test

equipment AD 3050 TFAE0017

#### 3 Introduction

This guide has been produced to aid the splice designer and user of TE Connectivity QSZH-125 adhesive lined tubing to select the most appropriate size and installation conditions to produce optimum results for an environmentally sealed splice.

The document has three main sections:

Section 4 Splice Design and Preparation Guidelines Section 5 Tube size selection and installation guidelines

Section 6 Sealing verification guidelines

NB: The recommendations presented here are based on general industry information. Since TE Connectivity does not have knowledge of the specific application and the end use conditions of all users, each user should determine the correct size of tubing together with the installation conditions for their own application and evaluate the splice against individual requirements.

(Refer to TE Connectivity to ensure latest issue of this document).

No:	PIP-101	Revision:	2	Dated:	January 2012
-----	---------	-----------	---	--------	--------------

#### 4 Splice Design and Preparation Guidelines

#### 4.1 Splice Design

There are many factors, which can influence the successful installation of a heat shrink sleeve for splice sealing. These include:

- i) total number of wires;
- ii) number difference of wires between each side;
- iii) cumulative insulation cross-sectional area;
- iv) cumulative insulation cross-sectional area difference between each side.

Generally for splices having no more than 4 wires per side the installation and sealing characteristics are excellent.

For splices having 5 to 7 wires per side the configuration is more complex and corresponding installation times are likely to be longer and the installation window smaller. Consequently, these splices may require additional work in establishing production installation conditions.

For optimum performance and compatibility it is recommended that T3 (125°C) rated wire be used and the following guidelines followed:

Parameter	Tubing Size					
	Nr 1	Nr 2	Nr 3	Nr3A	Nr 4	
Maximum number of wires per side	7	7	7	7	7	
Min./max. CSA range (mm²) NB1	1.3 to 12	3 to 20	5 to 35	15 to 60	30 to 85	
Preferred maximum CSA difference between sides of splice (mm <sup>2</sup> )	8	12	22	30	35	
Absolute maximum CSA difference between sides of splice (mm²)	11	14	28	40	50	

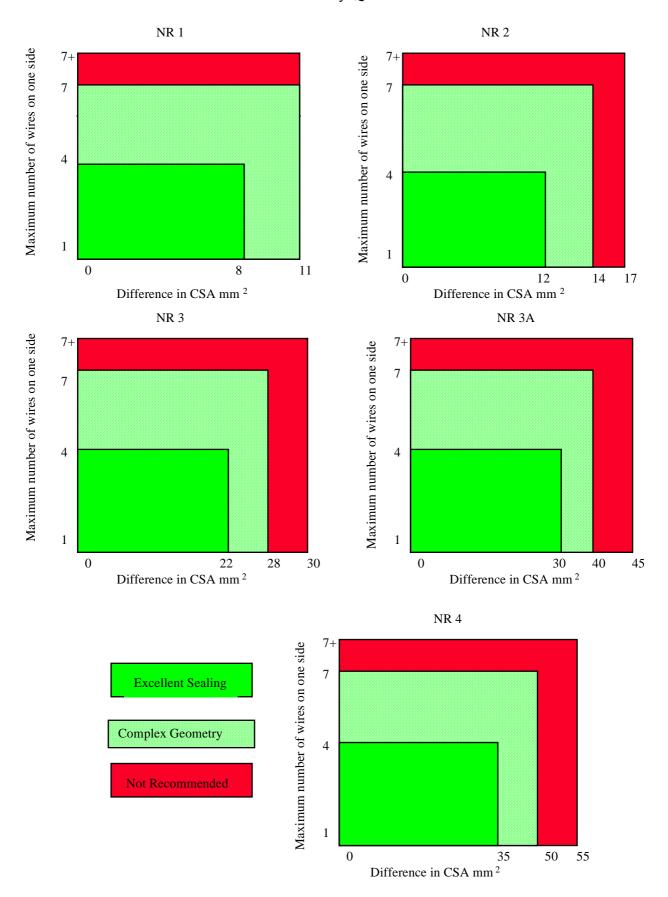
NB: See also the splice balancing matrix which pictorially shows additional guidelines with respect to both number of wires per side of splice and difference in CSA (cross sectional area).

NB 1: Due to variations in wire insulation thickness between manufacturers of similar gauge wires, the cross-sectional areas shown above relate to the cumulative areas of a splice using the outside diameter, of each wire insulation, in the calculation.

Splices outside of these recommendations will require extensive testing to ensure that reliable sealing of the splice can be consistently achieved.

No: PIP-101 Revision: 2 Dated: January 2012

#### SPLICE BALANCING MATRIX: TE Connectivity QSZH-125



No:	PIP-101	Revision:	2	Dated:	January 2012
-----	---------	-----------	---	--------	--------------

#### 4.2 **Splice Preparation Guidelines**

The splice can be constructed by conventional techniques such as resistance welding, ultrasonic welding, or mechanical crimping or "clip and dip". The strands of the conductor must be completely captured in the nugget or crimped area. There should be no loose strands, especially those pointing upwards which could "poke-through" the tubing material during installation.

It is important to ensure that the distance from the welded nugget or crimp, to the wire insulation is  $3.5 \pm 1.5$ mm to allow the adhesive sufficient space to flow and seal between the wires (see Figures 1 & 2). The copper wire strands from opposing sides of the splice must not compromise this dimension. Additionally, the wire around the splice should be essentially free of dirt, oil, solder, flux and moisture for optimum performance.

Figures 1 & 2 (see over)

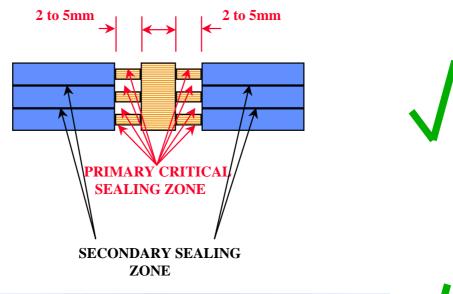
No:	PIP-101	Revision:	2	Dated:	January 2012
-----	---------	-----------	---	--------	--------------

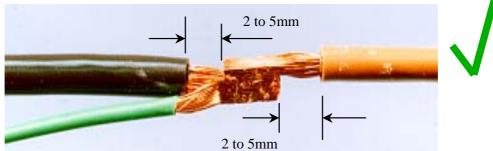
Figure 1

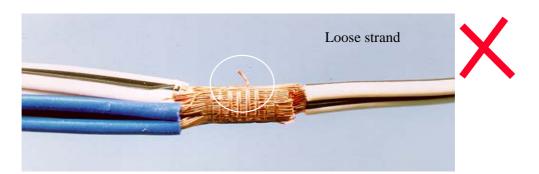


**QSZH-125** 

# Splice preparation guidelines (Ultra sonic welded splices)







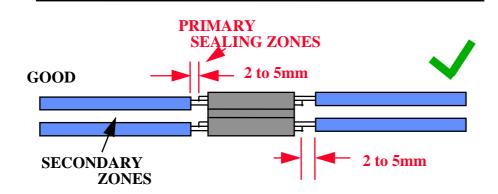
No:	PIP-101	Revision:	2	Dated:	January 2012
-----	---------	-----------	---	--------	--------------

Figure 2

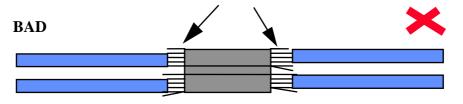


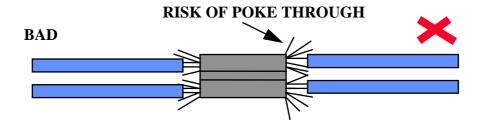
# **QSZH-125**

# Splice preparation guidelines (Crimped splices)



#### **EXCESS OVERLAP OF WIRE STRANDS**





No:	PIP-101	Revision:	2	Dated:	January 2012
-----	---------	-----------	---	--------	--------------

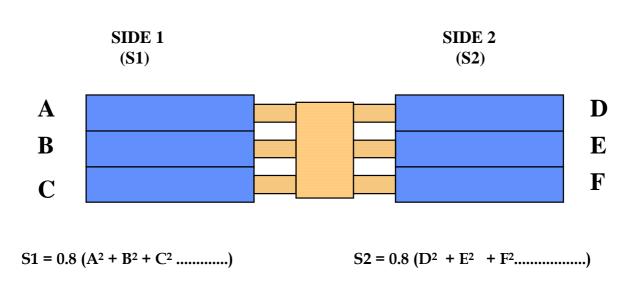
#### 5 Tube Size Selection and Installation Guidelines

#### 5.1 Tube Size Selection

Wire insulation diameters for a given gauge of wire can vary depending on the manufacturer. This will influence the cumulative cross sectional area of the wire bundle in the splice. A "general" chart showing nominal wire insulation OD (mm) and corresponding cross sectional areas (mm²) is given in this guide (Section 6). However, it is recommended that the simple calculation shown in 5.1.1 and Fig 3 be followed to determine the cumulative cross sectional area more accurately for each side of the splice.

# 5.1.1 Cumulative Cross Sectional Area

Figure 3



Where	S1 =	Cumulative area of side 1
	S2 =	Cumulative area of side 2
	A	Diameter of wire A
	В	Diameter of wire B
	C	Diameter of wire C
	D	Diameter of wire D
	E	Diameter of wire E
	F	Diameter of wire F

Note:  $\Pi/4 \approx 0.8$ 

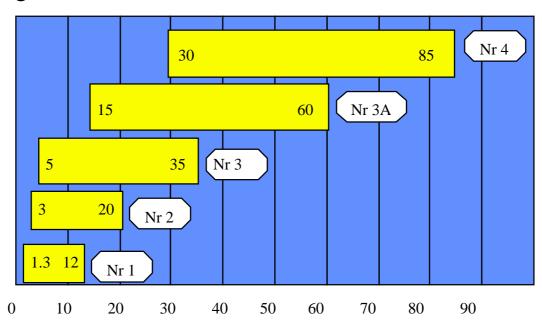
No:	PIP-101	Revision:	2	Dated:	January 2012
-----	---------	-----------	---	--------	--------------

#### 5.1.2 Tubing Size Range Table

When the cumulative areas for each side of the splice have been determined use the Table below to find the smallest tube size which can accommodate both values, e.g.:

NB: When mechanical crimping techniques are used it may be necessary to use the next largest tube size.

### **QSZH-125 TUBING SIZE RANGE TABLE**



Cumulative cross sectional area based on wire insulation OD (mm²)

No:	PIP-101	Revision:	2	Dated:	January 2012
-----	---------	-----------	---	--------	--------------

#### 5.2 **Installation Guidelines**

Installations can be carried out using various techniques including discrete or belt type heaters, the selected method being dependent on production area layout and required throughput. It is important that TE Connectivity installation equipment be maintained in a state of calibration using an UHI-250A thermal probe as described in the RBK-ILS-MK2 Processor Maintenance & Repair Manual THFIT/MR/020.

The installation "window" will be dependent on the set point temperature of the equipment, geometry and preparation of splice and the size of tubing. Generally the installation window will be small if the splice geometry is complex and the equipment set point high. For lower temperature set points the window will be larger but the corresponding installation time will be longer. Generally, it is recommended that discrete heaters such as the TE Connectivity RBK-Processor be set at 450 - 500°C, and the Model 19 belt heater at 550°C.

It is recommended that "heat" input as seen by the splice to be installed be measured via an UHI-250A Thermal Probe. (PCN: 288869, CLT-EQUIP-UHI-250A-PROBE. Refer to Appendix 2 for explanation of the Thermal Probe.)

Verification of sealed joints can be determined as outlined in Section 6.

#### 5.2.1 Installation Method

- 5.2.1.1 Determine tube size per section 5.1
- 5.2.1.2 Ensure installation equipment has been switched on for a minimum of 30 minutes to stabilize.
- 5.2.1.3 Recheck for loose wire stands and wire insulation cut back.

  Centrally locate the tubing onto the splice and position centrally within the heating zone of the application equipment. (See Figures 4 & 5)
- 5.2.1.4 Run the splice through the heating equipment; record the installation conditions, i.e. processor time/set point, or belt heater speed/set point. Run the UHI probe through at the same conditions to obtain the UHI temperature.
- 5.2.1.5 Increase the UHI probe temperature by 5-10°C increments by changing the processor time in 1-2 second steps or belt heater speed (not the set temperature) until the wire insulation or tubing jacket material shows visual signs of damage. (This is the upper limit of the installation window.).
- 5.2.1.6 Check all splices for sealing efficiency (0.5 bar air pressure per section 6). If the sample installed at the lowest UHI sealing temperature passes then lower the UHI probe temperature by 5° 10°C increments until a sealing failure occurs.
- 5.2.1.7 Prepare 5 sample splices at the minimum conditions, which gave a pass result when tested per section 6. If all 5 pass, this can be regarded as the lower limit of the installation window. If failures occur raise the UHI probe temperatures as previously until 5 from 5 pass to give the lower limit. If damage is seen before sealing is achieved, then the splice configuration may need re-designing.

In order to optimise sealing efficiency in a production environment it is recommended that the <u>mid</u> point between upper and lower limit be used.

No: PIP-101 Revision: 2 Dated: January 201	2
--	---

#### Note:

Sealing time for a given splice will depend on its complexity, number of wires and the wire type. In accordance with the above procedure the following times are offered as **approximate start points** for determining the installation window of a particular splice when using the following TE Connectivity Installation Equipment and may need to be adjusted up or down accordingly.

MK2 Processor Set Temperature 450°C – 500°C

	Time (seconds)
QSZH-125-NR1	7
QSZH-125-NR2	11
QSZH-125-NR3	12
QSZH-125-NR3A	15

Model 19 Belt Heater 550 Belt Speed

	Belt Speed
	Indicator setting
	(actual belt speed)
QSZH-125-NR1	600 (914mm/min)
QSZH-125-NR2	500 (762mm/min)
QSZH-125-NR3	400 (610mm/min)
QSZH-125-NR3A	300 (457mm/min)
QSZH-125-NR4	200 (305mm/min)

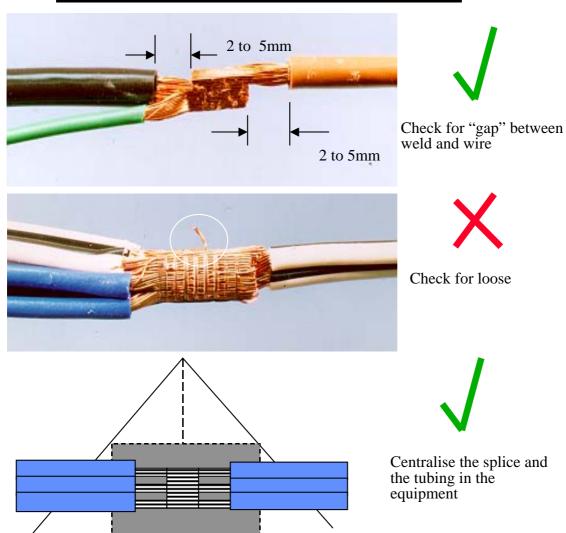
No:	PIP-101	Revision:	2	Dated:	January 2012
-----	---------	-----------	---	--------	--------------

Figure 4



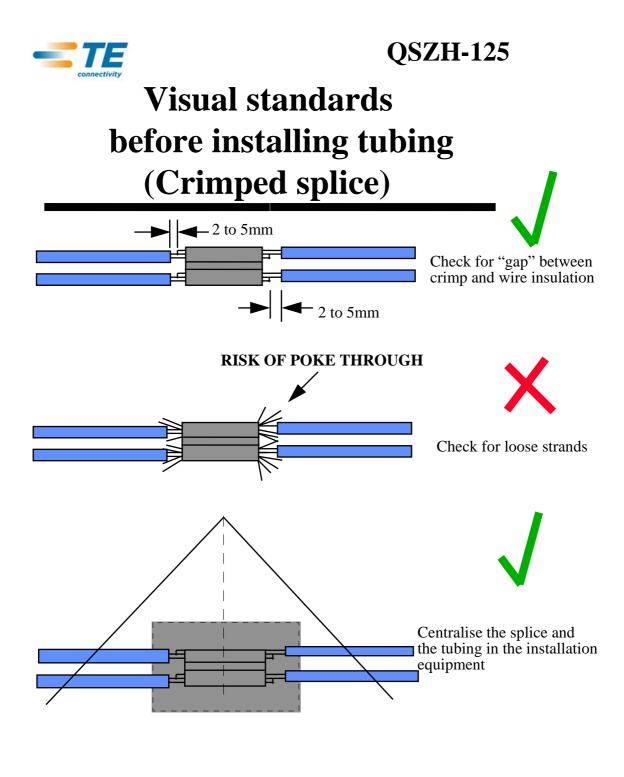
# **QSZH-125**

# Visual standards before installing tubing (Ultra sonic welded splices)



No:	PIP-101	Revision:	2	Dated:	January 2012
-----	---------	-----------	---	--------	--------------

Figure 5



No:	PIP-101	Revision:	2	Dated:	January 2012	
-----	---------	-----------	---	--------	--------------	--

#### 6 Sealing Verification / Visual Standards

#### 6.1 **Test Methods**

A variety of test methods exist which are incorporated by many major Automotive OEM's to determine the environmental integrity of an installed splice including:

- 1. Current Leakage
- 2. Insulation Resistance
- 3. Air Pressure
  - a) Not suitable for splices manufactured by "clip and dip".
  - b) Will not detect poke-through.

Refer to Appendix 3 for Test Methods.

For speedy determination of splice installation windows it is recommended that an air pressure test be used. Experience has shown excellent correlation between this method and Insulation Resistance/Current Leakage techniques for most types of splices.

TE Connectivity Seal Test equipment AD 3050 has been found to be acceptable (for details see TE Connectivity Flier No TFAE0017).

It can also be used to monitor sealing efficiency periodically throughout a production run.

Final verification should be per OEM specification.

No:	PIP-101	Revision:	2	Dated:	January 2012
-----	---------	-----------	---	--------	--------------

#### **Visual Standards 6.2**



# **QSZH-125**

# **Visual Standards** after Installation





Under installed



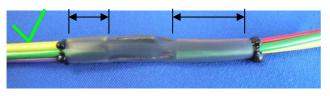
Over heat of tubing



3. Over heat of wires



Tubing off centre and wire exposed



**Tubing off centre (verify sealing)** 



Wire strand poke through



7. Acceptable

No:	PIP-101	Revision:	2	Dated:	January 2012
-----	---------	-----------	---	--------	--------------

# **Appendix 1: General Wire Chart**

	Approximate Cross Sectional Area based on wire insulation diameter (mm²)								
Nominal	Number of Wires								
OD (mm)	1	2	3	4	5	6	7		
1.4	2	3	5	6	8	9	11		
1.5	2	4	5	7	9	11	12		
1.6	2	4	6	8	10	12	14		
1.7	2	5	7	9	11	14	16		
1.8	3	5	8	10	13	15	18		
1.9	3	6	9	11	14	17	20		
2.0	3	6	9	13	16	19	22		
2.1	3	7	10	14	17	21	24		
2.2	4	8	11	15	19	23	27		
2.3	4	8	12	17	21	25	29		
2.4	5	9	14	18	23	27	32		
2.5	5	10	15	20	25	29	34		
2.6	5	11	16	21	27	32	37		
2.7	6	11	17	23	29	34	40		
2.8	6	12	18	25	31	37	43		
2.9	7	13	20	26	34	40	46		
3.0	7	14	21	28	35	42	49		
3.1	8	15	23	30	38	45	53		
3.2	8	16	24	32	40	48	56		
3.3	9	17	26	34	43	51	60		
3.4	9	18	27	36	45	54	64		
3.5	10	19	29	38	46	56	67		
3.6	10	20	31	41	51	61	71		
3.7	11	22	32	43	54	65	75		
3.8	11	23	34	45	57	68	79		
3.9	12	24	36	48	60	72	84		

No:	PIP-101	Revision:	2	Dated:	January 2012
-----	---------	-----------	---	--------	--------------

**Appendix 1: General Wire Chart (continued.)** 

	Approximate Cross Sectional Area								
	based on wire insulation diameter (mm²)								
Nominal	Number of Wires								
OD (mm)	1	2	3	4	5	6	7		
4.0	13	25	38	50	63	75	88		
4.1	13	26	40	53	66	79			
4.2	14	28	42	55	69	83			
4.3	15	29	44	58	73	87			
4.4	15	30	46	61	76				
4.5	16	32	48	64	80				
4.6	17	33	50	66	83				
4.7	17	35	52	69	87				
4.8	18	36	54	72					
4.9	19	38	58	75					
5.0	20	39	59	79					
5.1	20	41	61	82					
5.2	21	42	64	85					
5.3	22	44	66	88					
5.4	23	46	69						
5.5	24	48	71						
5.6	25	49	74						
5.7	26	51	77						
5.8	26	53	79						
5.9	27	55	82						
6.0	28	57	85						
6.1	29	58	87						
6.2	30	60							
6.3	31	62							
6.4	32	64							
6.5	33	66							
6.6	34	68							
6.7	35	70							
6.8	36	73							
6.9	37	74							
7.0	38	77							
7.1	40	80							
7.2	41	81							
7.3	42	84							
7.4	43	86							
7.5	44	88							
7.6	45	20							
7.7	46								
7.8	48								

No:	PIP-101	Revision:	2	Dated:	January 2012
-----	---------	-----------	---	--------	--------------

#### **Appendix 2: UHI-250A Thermal Probe**



### **UHI-250A (pcn 288869)**

The heat applied to a splice is conveniently measured by a TE Connectivity UHI-250A Thermal Probe. This Thermal Probe has a known mass of aluminium with fixed dimensions and a thermocouple embedded in the aluminium. The theory of use of the Probe is derived from the equation for calculating the quantity of heat required to raise a mass from one temperature to another.

$$Q = Mkc (t_2 - t_1)$$
Where  $Q = Quantity of Heat$ 
 $M = Mass$ 
 $k = units constant$ 
 $c = specific heat$ 
 $t_1 = ambient temperature$ 
 $t_2 = final temperature$ 

When using the probe, M, k, c and  $t_1$  are constant so that the final temperature (ignoring heat loss) is proportional to the quantity of heat.

$$t_2 = \infty O$$

The temperature rise of the aluminium is proportional to the heat received during the time the Probe is in the heat zone of the heater. By relating this temperature to the sealing performance of a given splice the window for this splice can be defined. The lower point is the lowest temperature at which the splice seals and the upper point the highest temperature at which no thermal damage is observed. The best probe temperature (quantity of heat) for a given splice is normally set at the midpoint of the window. This midpoint temperature is best determined in the manufacturing environment where the splice is to be sealed.

The UHI-250A Thermal Probe is available through your local TE Connectivity Office (PCN: 288869).

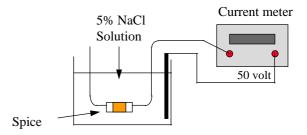
No:	PIP-101	Revision:	2	Dated:	January 2012	
-----	---------	-----------	---	--------	--------------	--

#### **Appendix 3: Test Methods**

#### **Current Leakage: Test Method**

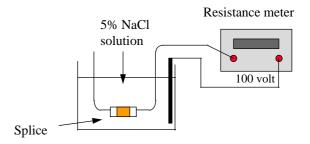
Immerse the centre section of the specimens in a water bath containing 5 percent by weight of sodium chloride  $(23 \pm 2^{\circ}C)$ .

Check for current leakage after 24 hours immersion. Applied test voltage is 50V dc. Take the reading after 60 seconds. The splice shall be considered sealed if current leakage is less than 0.25 micro amps



#### **Insulation Resistance: Test Method**

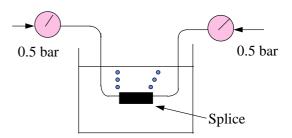
Immerse the centre section of the specimens in a water bath containing 5 percent by weight of sodium chloride (23 $\pm$  2°C). Check for Insulation Resistance after 24 hours immersion. Applied test voltage is 100V dc. Take the reading after 60 seconds. The splice shall be considered sealed if the Insulation Resistance is greater than 2 x 10 $^8$  ohm



#### **Air Pressure: Test Method**

Immerse the centre section of the specimens in a water bath. Connect both ends to a regulated air supply and apply 0.5 bar for 1 minute. If no bubbles arise from the splice area sealing is considered acceptable.

Final verification should be per OEM specification.



No:	PIP-101	Revision:	2	Dated:	January 2012
-----	---------	-----------	---	--------	--------------

### **Appendix 4: Trouble Shooting**

Fault	Possible Cause	Solution		
Sleeve not fully shrunk	Insufficient heat	Increase heat. Check UHI-250A		
onto splice	insufficient near	reading		
	Insufficient time	Increase time in heater element		
	2110 0122202010 022210			
	Wrong tube size selected	Re-assess tube selection		
Sleeve incorrectly	Incorrect location prior to	Locate correctly (offset tube		
positioned after	installation	accordingly)		
installation (milk-off)		Use alignment guide on heater		
	Splice unbalanced	Redesign splice if possible		
		Consult local TE Connectivity		
		representative		
Sleeve partially	Splice did not align centrally	Use guidelines on machine for		
recovered at one end	in application equipment	centralisation		
		Check calibration		
Sleeve or wire	Excessive heat	Reduce installation time or		
overheated		temperature		
		Check calibration		
Sleeve scorched on one	Excessive wire curvature	Use straightened wire		
side	Splice located incorrectly in	Reposition splice		
	machine			
Sleeve splits	Sharp edge of nugget/crimp	Check welder/crimp tooling		
	Wire strand loose	D 1 ' (11 (' ('		
	Excessive heat	Reduce installation time or		
	Wrong tube size selected	temperature Re-assess tube selection		
Wine strand poless	Wire strand loose from			
Wire strand pokes through tube	welding or crimp	Check welder/crimp tooling Check splice construction		
Cannot seal splice	Inadequate heat	Increase installation time or		
Carmot sear sprice	madequate neat			
	Incorrect size of tube	temperature Refer to sizing guide		
	Too many wires	Reconstruct splice		
	Contamination on wires	Clean splice		
	Inadequate sealing zone	Check splice manufacturing		
		process		
		Check equipment calibration		
Wire damage at sleeve	Excessive heat	Reduce installation time or		
edge but sleeve visually		temperature		
OK	Splice not centered in	Use guides on machine		
	machine			
	Mismatch of tube/wire			
	Temperature rating			